Reduce down time

Hydraulic cylinders are used in many different applications in the mobile and industrial sectors; transferring loads through linear motion. High side load conditions can cause metal-on-metal contact of cylinder components to occur – critically damaging the rod, piston and bore – and result in leakage and costly equipment repair and down time.

Parker’s tight tolerance WPT and WRT Series wear rings in our 4778 material offer an internally lubricated surface, precision tolerances and best in class compressive modulus in a wear ring configuration that:
- Withstands deflection
- Reduces tolerance stack-up, and
- Maximizes resistance to side load

Contact our application engineers to learn more.

**Product Features:**
- Internally lubricated glass-filled nylon for low friction
- High compressive modulus to prevent metal-to-metal contact
- Chamfered corners hold tight against the gland for less interference and ease of installation
- Tight tolerance reduces tolerance stack-up and allows for precision fit of components with less dimensional play

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Side Loading

Smooth operation of a hydraulic cylinder depends on symmetrical forces. Side loading occurs when bending or an uneven force pushes the rod up, down or to the side during the stroke.

Side loading causes uneven wear on the piston as well as metal-to-metal contact between the piston and the bore as the piston is dragged across the internal walls of the cylinder. This sounds harmful, and it is — eventually scoring and damaging both the piston and cylinder bore, the rod and head glands — creating leak paths and potentially destroying the cylinder. The use of tight-tolerance wear rings made from materials with a high compressive stress rating can help prevent side loading and reduce poor cylinder performance and down time.

Compressive Stress (Modulus)

Compressive stress is a better indicator of a wear ring material’s ability to prevent metal-to-metal contact than maximum compressive strength.

Here’s Why

Wear ring materials are traditionally compared against each other based on their respective mechanical property value of maximum compressive strength. The generally accepted test method for determining maximum compressive strength for wear ring materials is ASTM D695. Parker asserts that maximum compressive strength regarding wear ring materials is a misapplied indicator of a material’s ability to prevent metal-to-metal contact in application, because in the ASTM D695 test method, maximum compressive strength values are achieved well beyond the point in which metal-to-metal contact is experienced in hydraulic cylinders. Think of it as evaluating the effectiveness of a car bumper in resisting cosmetic damage by measuring the size of cracks created in an engine block.

Seriously, though, we propose the better indicator of a wear ring material’s ability to prevent metal-to-metal contact is its compressive stress (compressive modulus), which measures how much force it takes to compress the material a specified distance. ASTM recognizes this very point in its published synopsis for “Significance and Use” of ASTM D695.¹

Test Subject Material Samples

All tests were performed using wear rings that had a nominal 1.25” ID, were 0.25” wide with a 0.125” thick radial cross section. The material compounds tested are identified as shown:

Our Analysis

We wanted to identify which, among a variety of commercially available wear ring materials, had the best compressive strength (modulus) property — as an indicator in preventing metal-to-metal contact under the highest loads.

Parker designed a custom compressive stress test fixture for an Instron® test stand with an environmental chamber to test a variety of materials (Figure 2, shown with Parker wear ring in 4733 material).

Wear Ring Groove Calculations

For a cylinder rod or piston wear ring application the tolerance stack-up to achieve metal-to-metal contact ranges from 0.005” and 0.009”. These calculations do not take into consideration angularity of the rod and piston relative to the cylinder head and cylinder tube or any rod bending. With rod angularity or rod bending, the metal-to-metal clearance is less. Examples of rod gland calculations are shown below:

1. Parker Materials
   a) 4733
   b) 4650
   c) 4778
2. Manufacturer S
   a) S1
   b) S2
3. Manufacturer H
   a) H
4. Manufacturer T
   a) T1
   b) T2
5. Manufacturer P
   a) P1
   b) P2

Compression Test Equipment

1. Custom wear ring compressive modulus fixture designed by Parker (shown in Figure 2)
2. Instron® test stand with environmental chamber

Test Procedure

1. The wear ring was cut in half across its circumference and one half was placed onto the center of the fixture to compress the radial cross-section of the wear ring.
2. The Instron head compressed the sample 0.050” at a rate of 0.002”/sec.
3. The reaction force was recorded every 0.0005” traveled at both temperatures
4. A matching control wear ring shape made of 6061-T6 aluminum was used to determine fixture and hardware deflections at both test temperatures. This deflection was subtracted from the measured wear ring displacement to show an accurate displacement rate.
5. Six wear ring halves were tested for each material; three at 23°C (room temperature) and three at 100°C. The median curve is shown for each material on Graphs 1-4 in Figure 4 on the following page.

A critical performance measurement is the distance a wear ring can compress in a cylinder before metal-to-metal contact is observed. It was calculated that metal-to-metal contact will occur when a wear ring is deflected between a minimum distance of .005” and a maximum of .009” based on tolerance stack ups using tight tolerance wear rings.

Wear Ring Groove Calculations

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### Rod Wear Ring Examples For Minimum and Maximum Allowable Displacement

**Best case stack-up (Reference Fig 3 below):**

\[
\text{Min. C1} - (\text{Max. B1} - 2 \times \text{Minimum Wear Ring cross-section})/2 = \\
\frac{2.017 - (2.253 - 2 \times 0.123)}{2} = 0.005"
\]

**Worst case stack-up (Reference Figure 3 below):**

\[
\text{Max. C1} - (\text{Min. B1} - 2 \times \text{Maximum Wear Ring cross-section})/2 = \\
\frac{2.019 - (2.251 - 2 \times 0.125)}{2} = 0.009"
\]

---

**Figure 3: Gland Calculations**

<table>
<thead>
<tr>
<th>Rod</th>
<th>A1 Rod Dia</th>
<th>B1 Groove Dia</th>
<th>C1 Throat Dia</th>
<th>D Groove Width</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>+0.000/-0.002</td>
<td>+0.002/-0.000</td>
<td>+0.002/-0.000</td>
<td>+0.010/-0.000</td>
</tr>
<tr>
<td></td>
<td>2.000</td>
<td>2.251</td>
<td>2.017</td>
<td>D=W + 0.010&quot;</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Piston</th>
<th>A Bore Dia</th>
<th>B1 Groove Dia</th>
<th>C1 Piston Dia</th>
<th>D Groove Width</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>+0.002/-0.000</td>
<td>+0.000/-0.002</td>
<td>+0.000/-0.002</td>
<td>+0.010/-0.000</td>
</tr>
<tr>
<td></td>
<td>2.000</td>
<td>1.749</td>
<td>1.983</td>
<td>D=W + 0.010&quot;</td>
</tr>
</tbody>
</table>
**Test Results**
Compressive stress test results of competitive wear ring materials at minimum and maximum allowable deflection show Parker’s 4778 wear rings withstand more load than most of the competition at room temperature and more load than all of the competition at operating temperatures.

**Conclusion**
With wear ring materials, compressive modulus is more relevant in real world applications than compressive strength (as defined by ASTM D695) in preventing metal-to-metal contact because reported maximum compressive strength of a material occurs well after a cylinder rod or piston would make contact with the respective cylinder gland or tube. In the functional operating range of a wear ring used in a hydraulic cylinder (0.005” to 0.010” displacement) materials with a stiffer compressive modulus will resist metal-to-metal contact best. Compressive modulus and compressive strength values reduce significantly when these properties are evaluated at 100°C compared to room temperature; meaning the higher temperature is a more critical evaluation.

**Figure. 4: Test Result Graphs.** Test results show that Parker’s 4778 material exhibits the highest compressive modulus of the group at the elevated temperature and second highest at room temperature at the minimum (.005”) and maximum (.010”) allowable displacement. At elevated temperature (100°C), Parker’s 4733 material has the next best compressive properties and is closely followed by materials T1 and T2.